

# Effect of Microporous Corundum Aggregates on Thermal Shock Resistance of Corundum Spinel Castables for Setting Block

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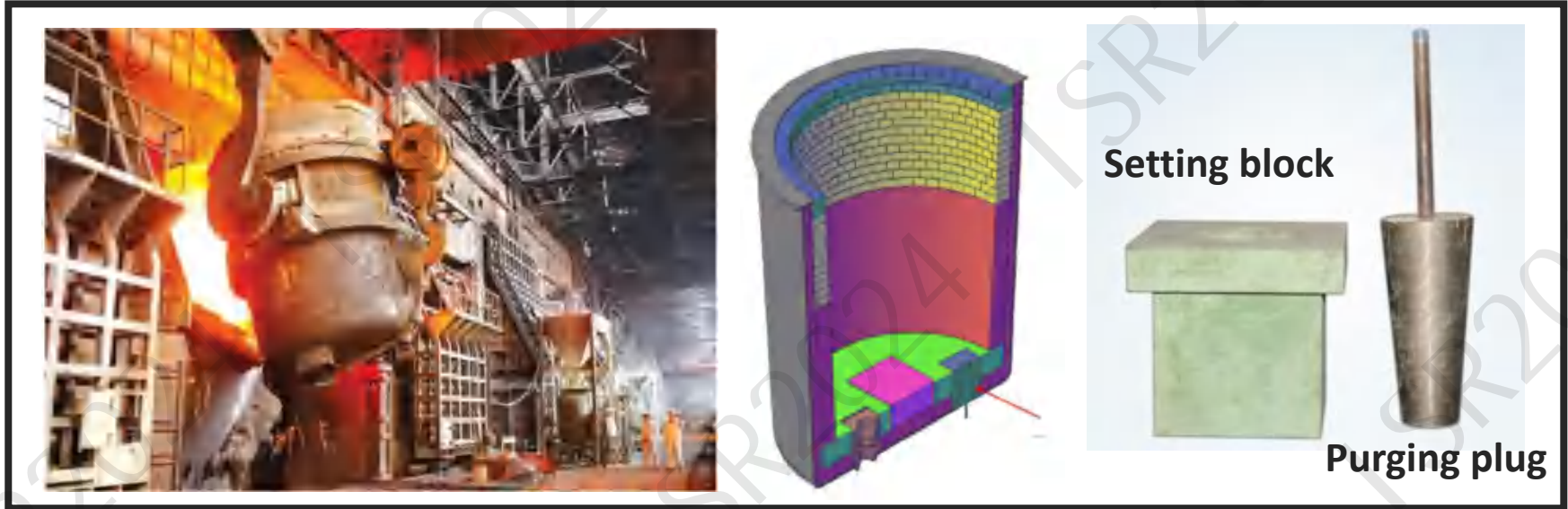
**1 Introduction**

**2 Experimental Procedures**

**3 Results and Discussions**

**4 Conclusions**

# 1. Introduction



**High temperature**  
**Long time refining**  
**Harsh service environment**

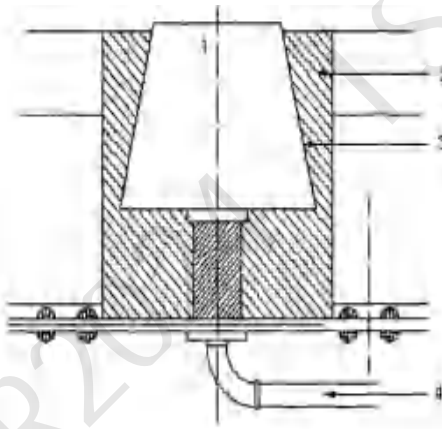
**Ladle refractory general contracting mode**



**Long service life**  
**High security**  
**Eco-friendly**

# 1. Introduction

## Setting block



1. Purging plug  
2. Setting block

### Service environment

- 1650°C~1680°C high temperature steel erosion
- Frequent thermal shocks
- Ferro-static pressure in dynamic condition
- Expansion stress from the bottom of the ladle

**Thermal  
shock**

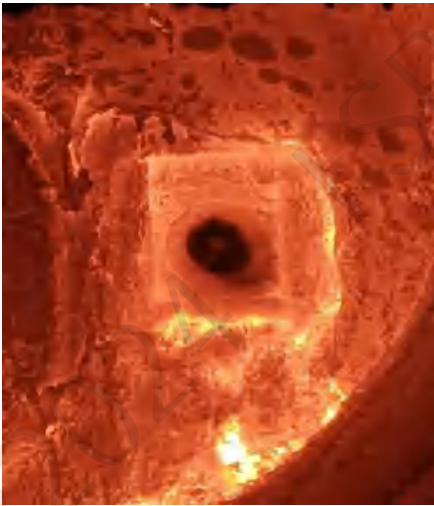
**Mechanical  
erosion**

**Chemical  
corrosion**

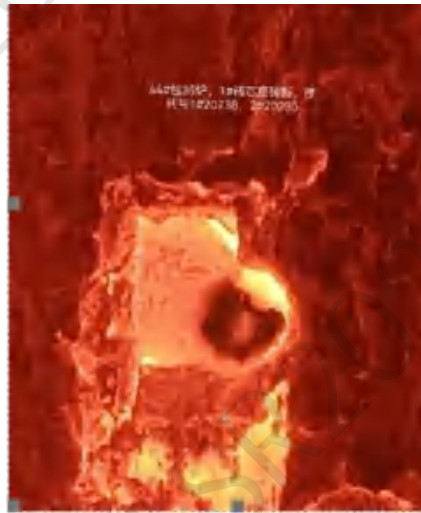
**Harsh service environment → good comprehensive performance**

# 1. Introduction

## Damage of setting block



Enlarged hole caused by wear and erosion



cracking and spalling



Broken and fracture

## Materials of setting block



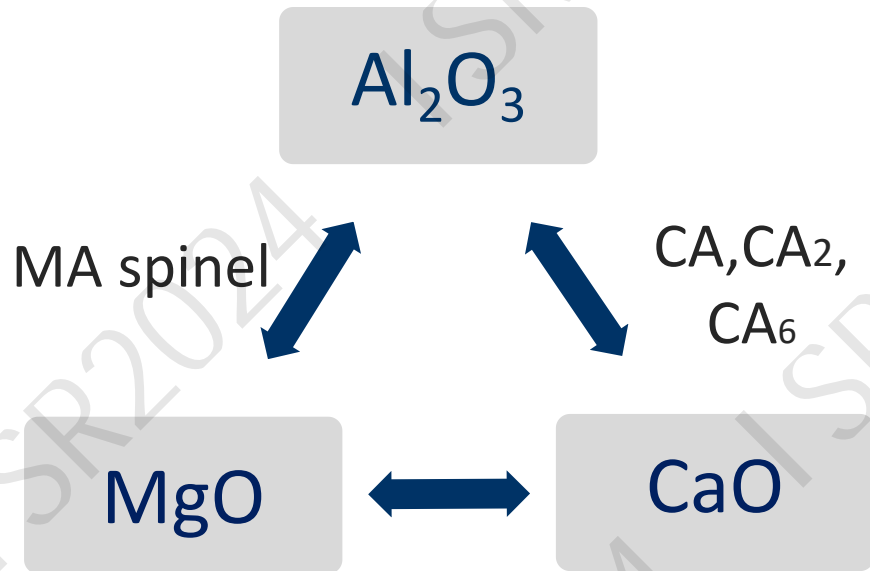
- ✓ Thermal shock resistance
- ✓ Volume stability
- ✓ Mechanical strength
- ✓ Slag resistance



**Castables of  
 $\text{Al}_2\text{O}_3\text{-MgO-CaO}$   
system**

# 1. Introduction

## Al<sub>2</sub>O<sub>3</sub>-MgO-CaO system



- High refractoriness under load
- Excellent corrosion resistance in steel/slag environments
- High oxidation resistance and chemical stability
- Relatively low fracture energy and unsatisfactory thermal shock performance

**Problem: thermal shock resistance**





# 1. Introduction

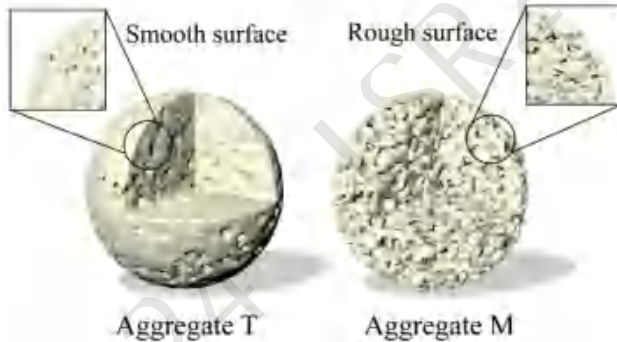
## Measures to improve thermal shock resistance

|  |  |   |
|--|--|---|
| <p>1. Increase the thermal conductivity of the material and reduce the thermal expansion coefficient of the material</p> <ul style="list-style-type: none"> <li>• Add non-oxide, B<sub>4</sub>C, SiC, Sialon, etc</li> </ul> | <p>2. Improve the strength of the material, while reducing the elastic modulus of the material, so that G/E is increased</p> <ul style="list-style-type: none"> <li>• Appropriately improve the porosity of the material, add fiber</li> </ul> | <p>3. Control the micro-structure of the materials</p> <ul style="list-style-type: none"> <li>• Micropores and micro-cracks are introduced, control the grain size</li> </ul> |
| <ul style="list-style-type: none"> <li>• Problem: High cost, introduction of impurities</li> </ul>   | <ul style="list-style-type: none"> <li>• Problem: Difficult to control</li> </ul>  | <ul style="list-style-type: none"> <li>• Problem: Difficult to control</li> </ul>   |

**How to improve thermal shock resistance on the premise of ensuring strength and slag resistance?**

# 1. Introduction

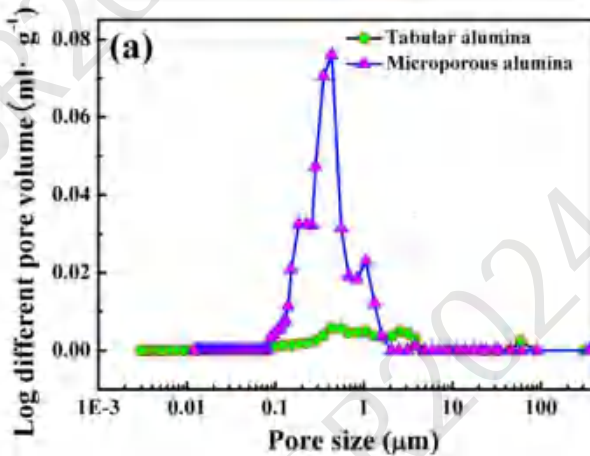
## Microporous corundum aggregate is introduced



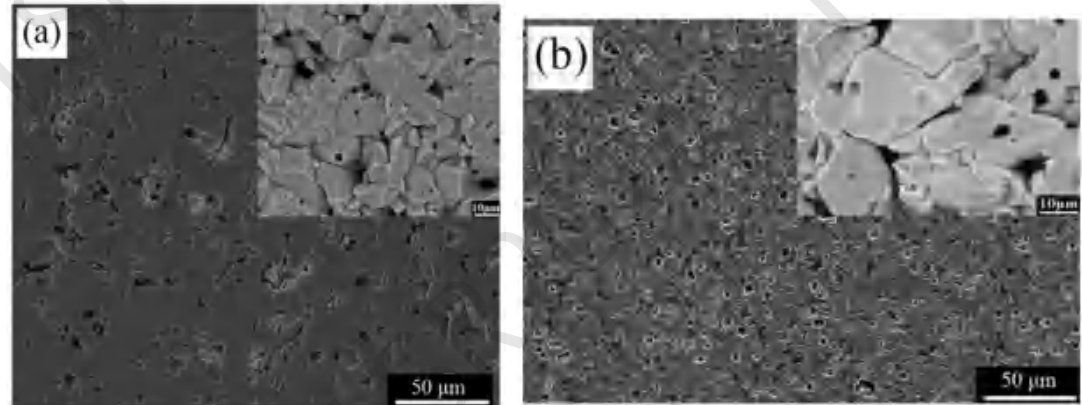
Physical indexes of different aggregates

|                     | AP(%) | BD(g/cm <sup>3</sup> ) | PSD(μm) |
|---------------------|-------|------------------------|---------|
| Tabular alumina     | 6.2   | 3.54                   | 9.77    |
| Microporous alumina | 25.7  | 2.82                   | 4.20    |

Diagram of different corundum aggregates



Pore size distribution of different corundum aggregates



Microstructure of different corundum aggregates



# 1. Introduction

## Application of microporous corundum aggregate in castable

Properties of two alumina–magnesia castables.

|                                       | Permanent linear change (%) |         | Apparent porosity (%) |         |         | Bulk density (g cm <sup>-3</sup> ) |         |         |
|---------------------------------------|-----------------------------|---------|-----------------------|---------|---------|------------------------------------|---------|---------|
|                                       | 1000 °C                     | 1500 °C | 110 °C                | 1000 °C | 1500 °C | 110 °C                             | 1000 °C | 1500 °C |
| Common alumina–magnesia castable      | -0.055                      | +0.934  | 19.8                  | 22      | 21.8    | 2.94                               | 2.92    | 2.92    |
| Lightweight alumina–magnesia castable | -0.025                      | +0.325  | 21.2                  | 24.7    | 22.7    | 2.89                               | 2.83    | 2.82    |

Strengths of two alumina–magnesia castables.

|                                       | Cold modulus of rupture (MPa) |         |         | Cold crushing strength (MPa) |         |         |
|---------------------------------------|-------------------------------|---------|---------|------------------------------|---------|---------|
|                                       | 110 °C                        | 1000 °C | 1500 °C | 110 °C                       | 1000 °C | 1500 °C |
| Common alumina–magnesia castable      | 2.8                           | 3.8     | 13.5    | 14.4                         | 18.19   | 74.38   |
| Lightweight alumina–magnesia castable | 4.01                          | 5.64    | 15.5    | 28.58                        | 36.58   | 78.75   |

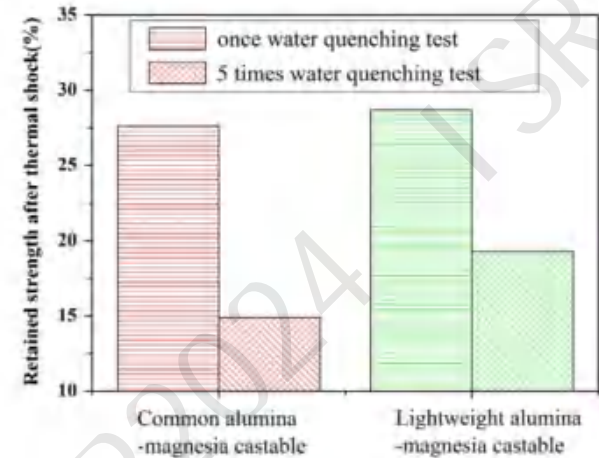
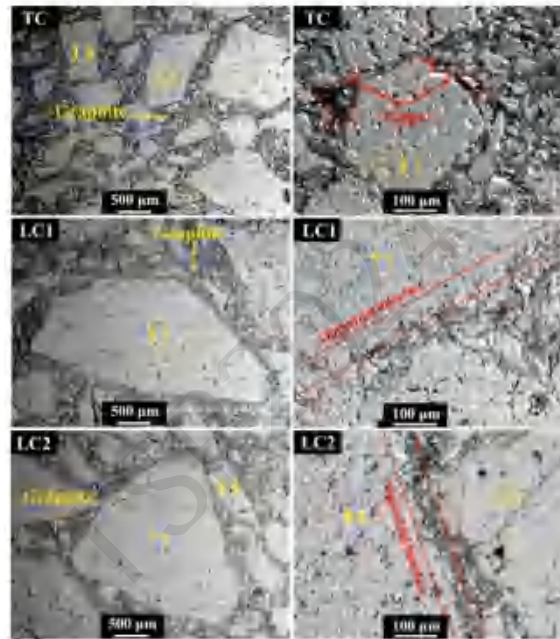
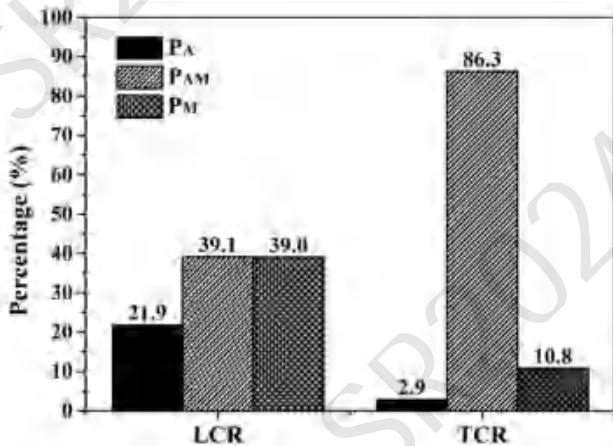
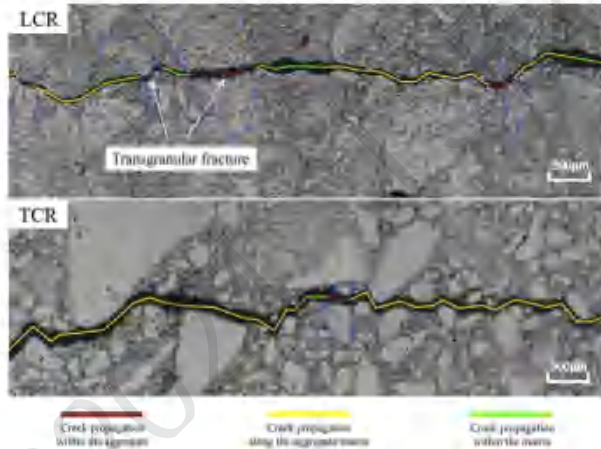


Fig. 4. Retained strength after thermal shock of different castables.

- Good volume stability
- High strength
- Proper porosity
- High thermal shock resistance

# 1. Introduction

## Application mechanism of microporous corundum aggregate



Tight bonding between the aggregate and matrix

**Intergranular fracture**



**Transgranular fracture**

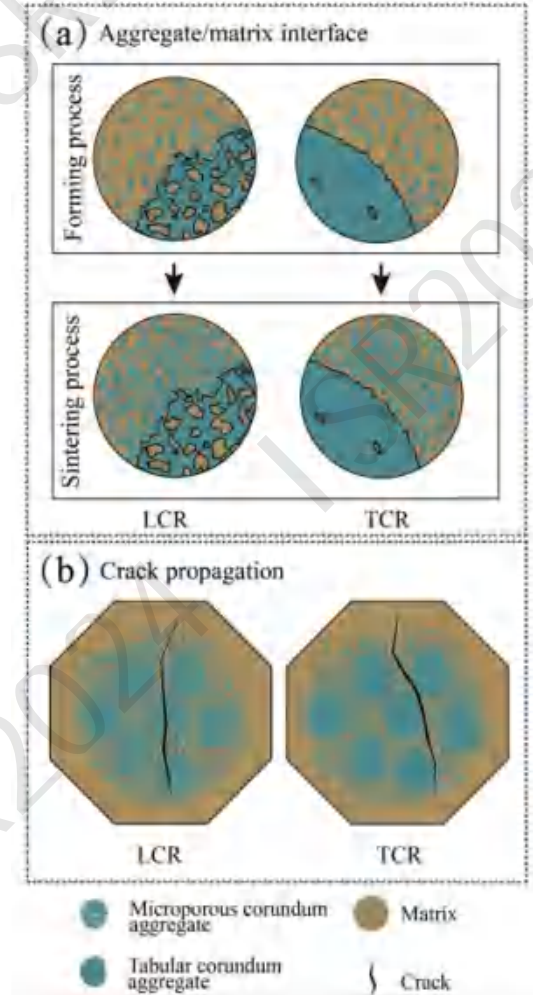


Fig. 9. Percentages of the three crack propagation mechanisms in the LCR and TCR specimens during three-point bending test.

# 1. Introduction

## Potential risk

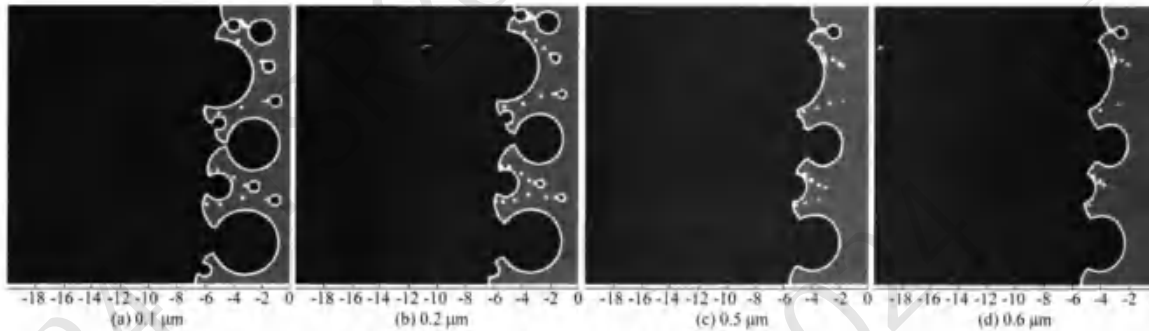


图1 熔渣对不同孔径骨料的耐火材料的渗透情况  
Fig. 1 Penetration results of slag to refractories with different aggregates

**Slag  
resistance?**

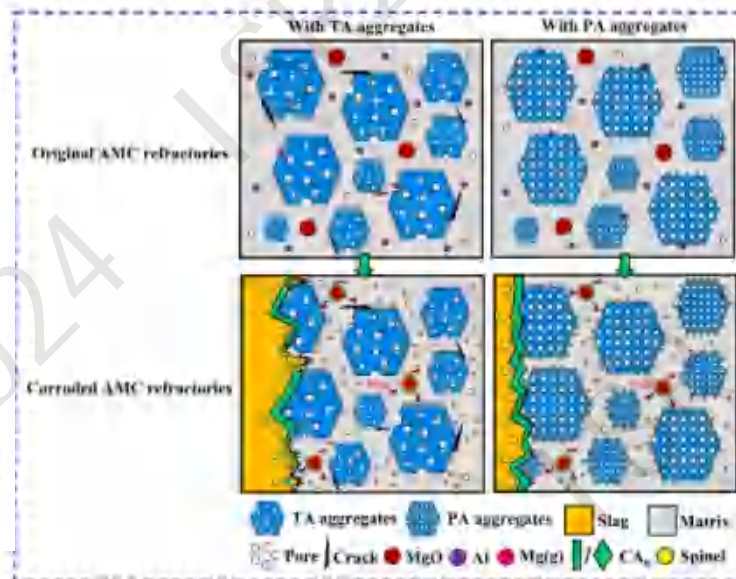
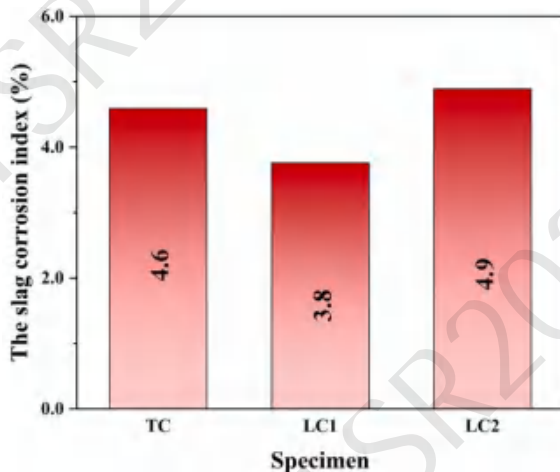


Fig. 13. The schematic diagram of original and corroded AMC refractories.

Interfacial cracks and  
matrix pores decreased

The hot surface forms  
a dense and continuous  
CA<sub>6</sub> isolation layer

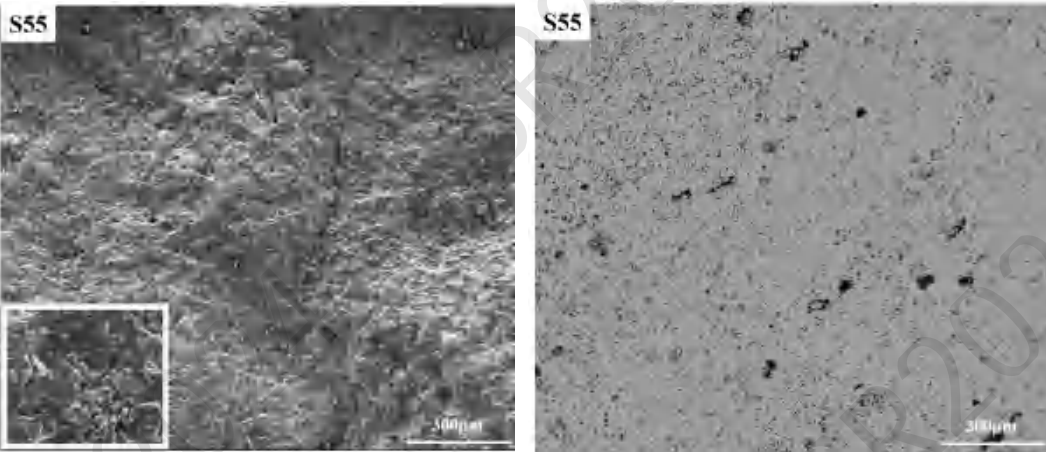
## Feasibility of application of microporous corundum aggregate in setting block

- **Ensure the basic performance of castable**
- **Improve thermal shock stability of materials**
- **Reduce raw material costs**

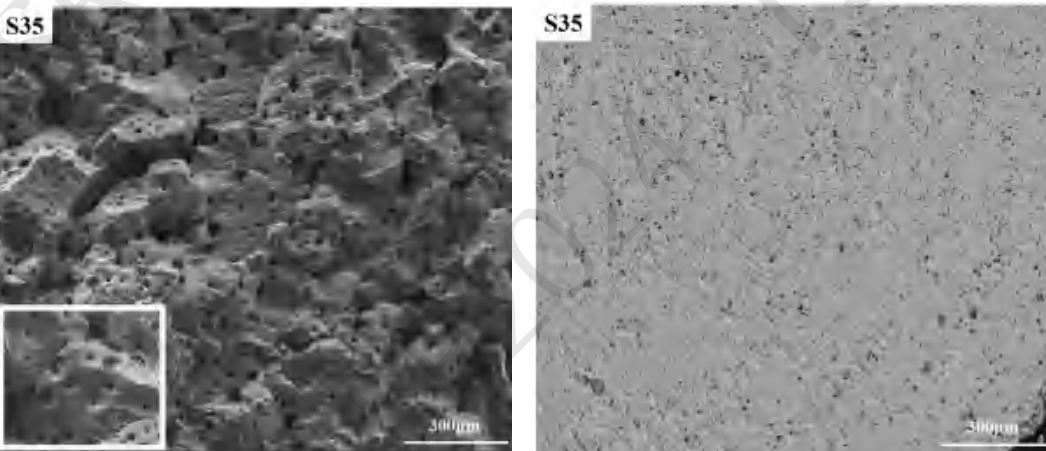


## 2. Experimental Procedures

### Comparison of corundum aggregate



Fracture surface of different aggregates



Polished surface of different aggregates

Physical properties of different aggregates

|     | Bulk density (g/cm <sup>3</sup> ) | Apparent porosity (%) | Water absorption (%) | True density (g/cm <sup>3</sup> ) |
|-----|-----------------------------------|-----------------------|----------------------|-----------------------------------|
| S55 | 3.60                              | 3.7                   | 1.0                  | 3.90                              |
| S35 | 3.40                              | 7.6                   | 2.2                  | 3.87                              |

#### S35

- Lower bulk density
- Higher AP and water absorption
- Rougher surface with sharp edges
- More homodispersed smaller pores

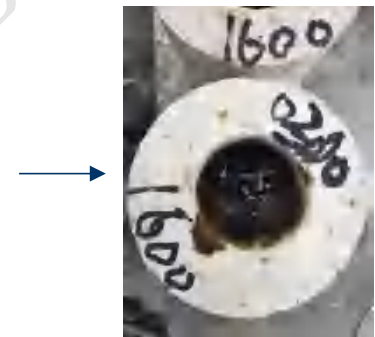
## 2. Experimental Procedures

### Experiment

Batches composition of castables

|          |         | Ref | MPA1 | MPA2  | MPA3 | MPA4 |
|----------|---------|-----|------|-------|------|------|
| S55      | 5~3mm   | 35  | 35   | 35    |      |      |
|          | 3~1mm   | 15  | 15   |       | 15   |      |
|          | 1~0mm   | 20  |      | 20    | 20   |      |
| S35      | 5~3mm   |     |      |       | 35   | 35   |
|          | 3~1mm   |     |      | 15    |      | 15   |
|          | 1~0mm   |     | 20   |       |      | 20   |
| S55      | 320mesh |     |      | 14    |      |      |
| Spinel   |         |     |      | 6     |      |      |
| AMA20    |         |     |      | 5     |      |      |
| Secar 71 |         |     |      | 5     |      |      |
| Additive |         |     |      | + 0.4 |      |      |

Curing(25°C )  
 Drying(110°C )  
 Firing(1100 °C,1600 °C)





## 3. Results and Discussions

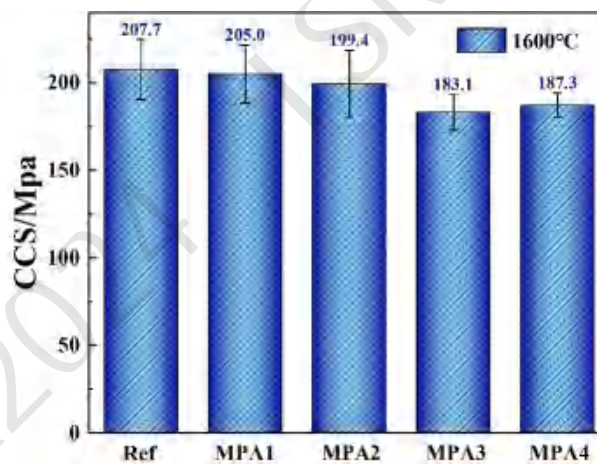
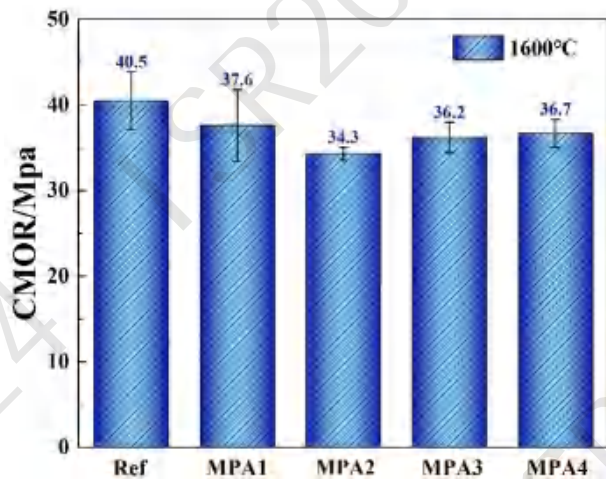
### Conventional performance

Properties of specimens treated at different temperatures

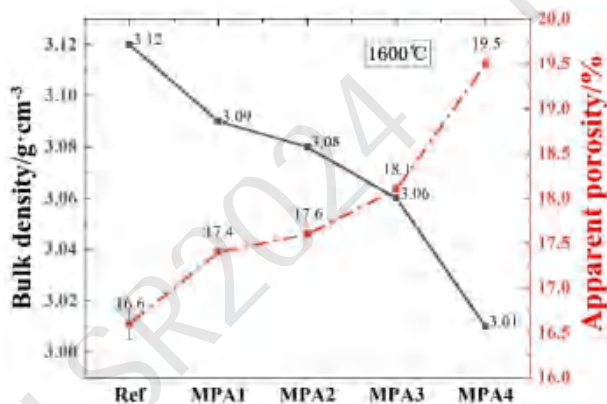
|                        | Ref   | MPA1  | MPA2  | MPA3 | MPA4  |
|------------------------|-------|-------|-------|------|-------|
| Water(wt%)             | 4.25  | 4.6   | 4.65  | 4.8  | 5.0   |
| Fluidity(mm)           | 240   | 245   | 240   | 230  | 245   |
| 110°C                  |       |       |       |      |       |
| PLC(%)                 | -0.14 | -0.01 | -0.06 | 0.00 | -0.04 |
| AP(%)                  | 7.7   | 10.9  | 10.7  | 11.1 | 10.6  |
| BD(g/cm <sup>3</sup> ) | 3.24  | 3.21  | 3.22  | 3.22 | 3.08  |
| CMOR(MPa)              | 15.8  | 16.6  | 16.2  | 14.1 | 15.4  |
| CCS(MPa)               | 109.2 | 102.3 | 103.5 | 96.1 | 92.3  |
| 1100°C                 |       |       |       |      |       |
| PLC(%)                 | 0.06  | 0.09  | 0.10  | 0.00 | 0.05  |
| AP(%)                  | 14.4  | 14.9  | 14.5  | 15.0 | 17.4  |
| BD(g/cm <sup>3</sup> ) | 3.15  | 3.13  | 3.14  | 3.13 | 3.02  |
| CMOR(MPa)              | 15.9  | 14.6  | 13.6  | 13.2 | 15.8  |
| CCS(MPa)               | 106.1 | 94.8  | 84.9  | 87.0 | 89.2  |

# 3. Results and Discussions

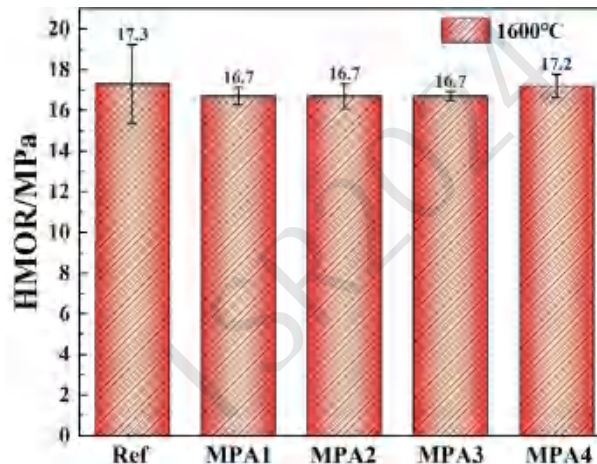
## Conventional performance



CMOR and CCS of specimens treated at 1600°C



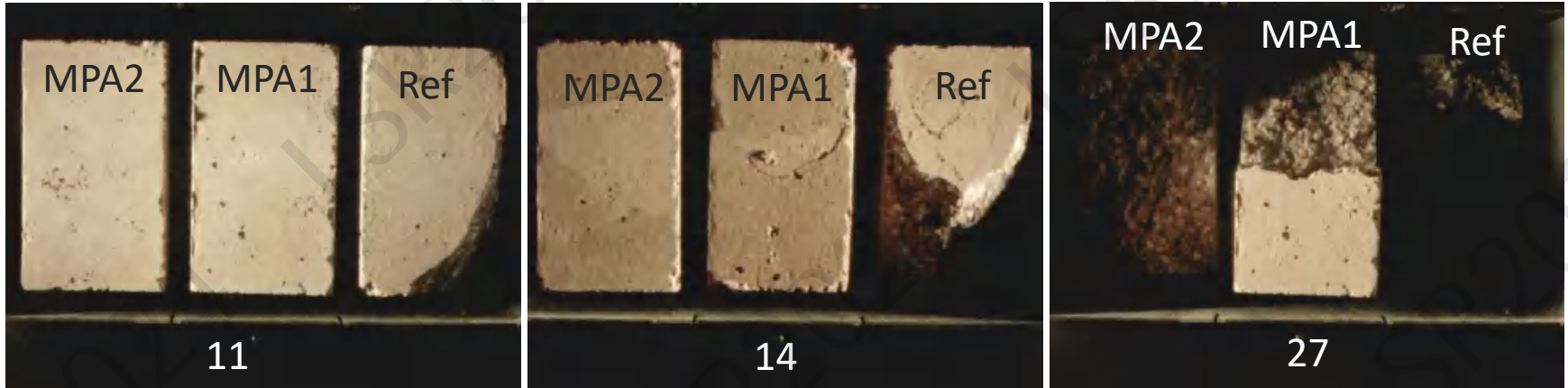
BD and AP of specimens treated at 1600°C



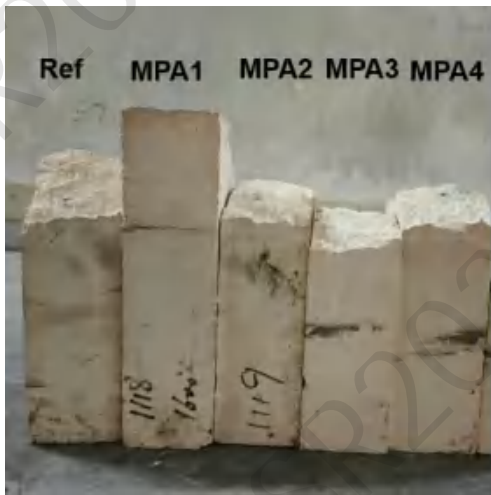
HMOR(1500°C×0.5h) of specimens treated at 1600°C

# 3. Results and Discussions

## Thermal shock test



Images during thermal shock test



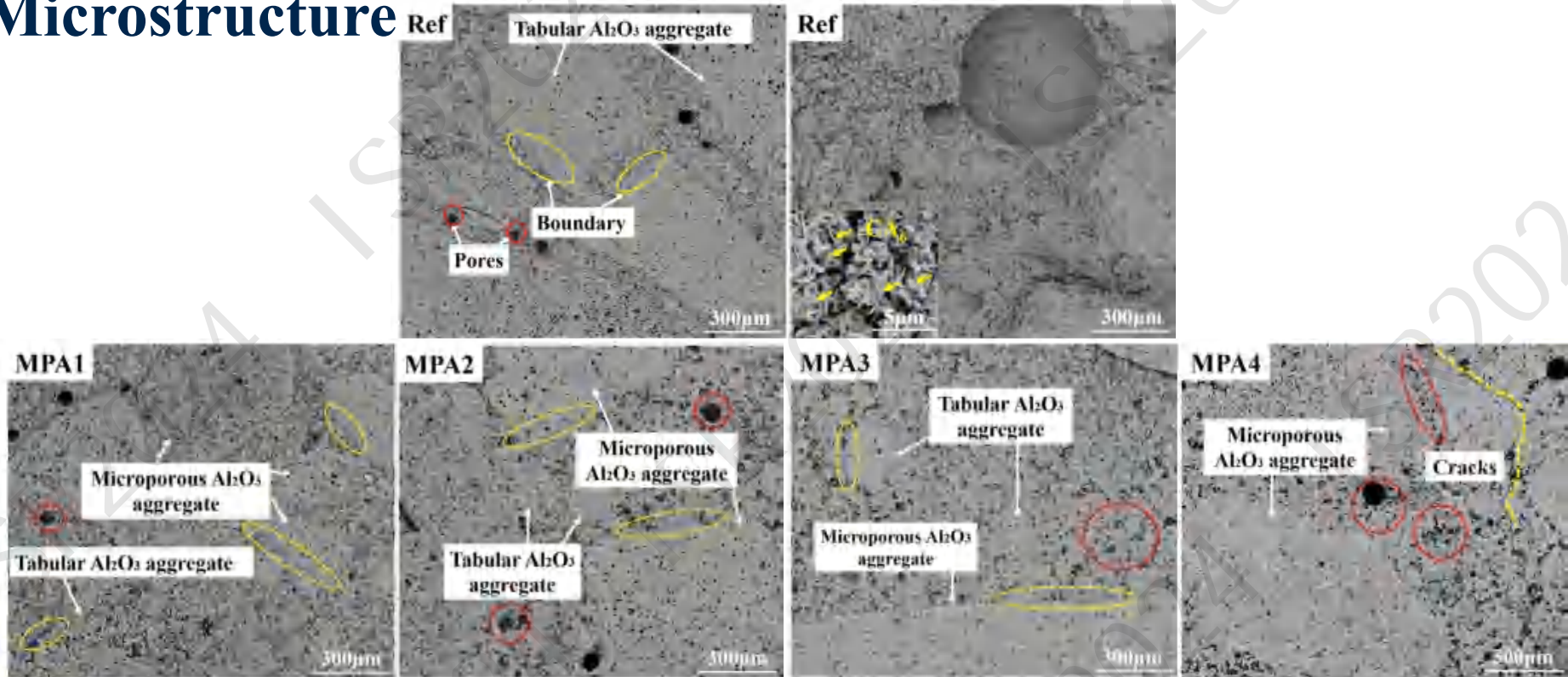
Images after thermal shock test

Thermal shock times of different specimens

|       | Ref | MPA1 | MPA2 | MPA3 | MPA4 |
|-------|-----|------|------|------|------|
| Times | 18  | 27   | 24   | 20   | 16   |

# 3. Results and Discussions

## Microstructure



The SEM images of specimens fired at 1600°C

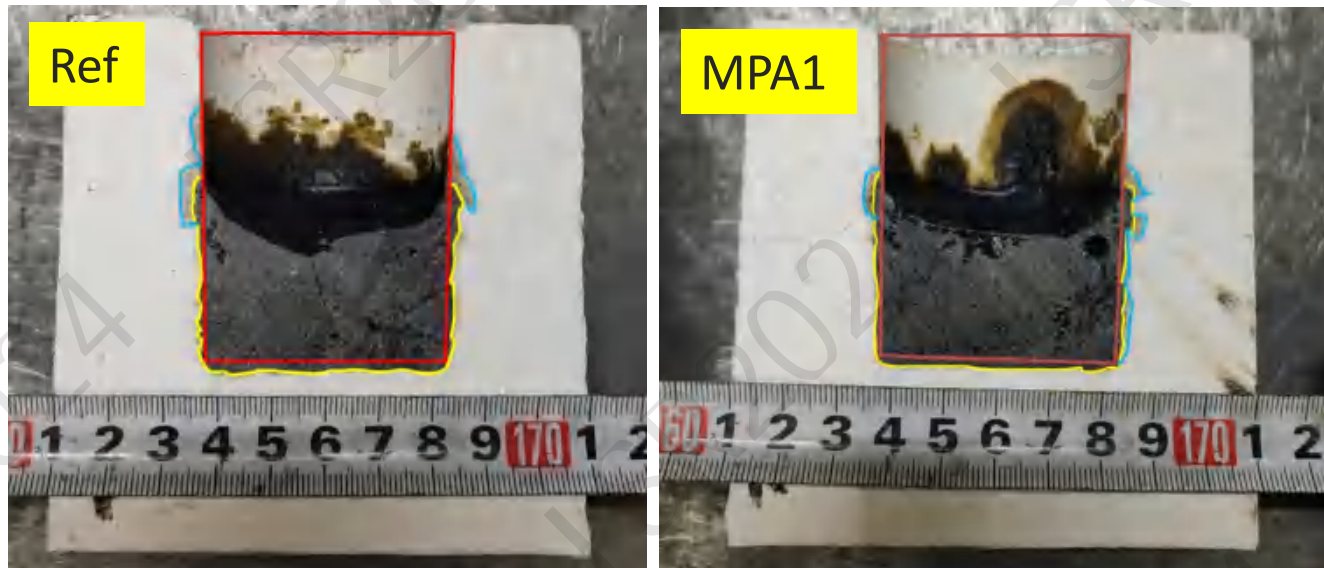
- MPA** Rough surface  
→ able to hang the slurry and better combine with the matrix
- Porous structure  
→ leading to more space to release the thermal stress

Strength

Thermal shock resistance



## Slag resistance



Cross-sections of Ref and MPA1 after slag corrosion test

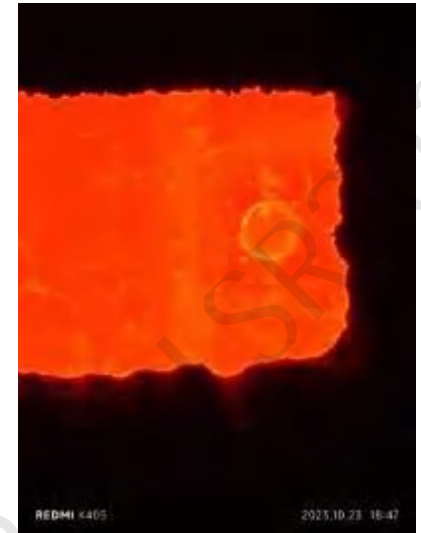
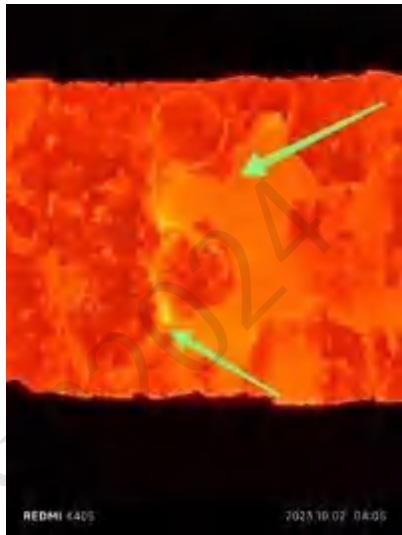
Corrosion and penetration index of Ref and MPA1 after slag corrosion test

|                     | Ref  | MPA1 |
|---------------------|------|------|
| Corrosion index/%   | 3.92 | 4.10 |
| Penetration index/% | 1.72 | 1.56 |

**No obvious difference**

## Industrial application

XX steel factory



Before (serious spalling)

After substitution of 10% 1-0mm microporous corundum aggregate

**The spalling and fracture of setting block have been decreased**



## 4. Conclusions

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The experimental results show that when the 1-0mm aggregate particles are completely replaced by microporous corundum aggregate, the specimens show best comprehensive performance, and the thermal shock resistance is increased by 50%. This is owing to the following reasons:

1. The rough surface of microporous aggregate can better combine with matrix, forming a dense bonding and improve the strength of castable.

2. The structure of microporous corundum aggregate and its higher water absorption increase the water requirement of castable and improve the porosity inside material, as a result the material has more space to accommodate and release the thermal stress in the state of dramatic temperature changes, thus improve their thermal shock resistance.

The use of microporous corundum aggregate is expected to solve the problem of fracture and spalling of setting block, it is of great significance for improvement of the lifetime for steel ladle, and bring out cost decreasing and benefit increasing.



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**Thanks for Your Attention!**